

Short Beam Strength Tests on Woven Composite Specimens

P.V. Joannette, A. Benkhelifa, J. Levesque, A. Gakwaya.

Department of mechanical engineering
Laval University
Quebec City, Canada

6th IC3 Arcachon, France, June, 4th 2018

Contents

- Introduction
- Material tested
- Experiment and results
- Finite element modeling
- FEA results
- Inverse problem
- Parameter identification algorithm
- Results from identification
- Conclusion

Introduction

- **Context**

CRIAQ project aimed at identifying material parameters for Progressive Damage and Failure analysis of woven composite composite under **tensile**, compressive, **shear**, bending and **impact loading**

- Material supplied by **Aerospace industrial** partners

- Testing, Analysis and Identification performed by **University partners** -

- **M3C Ulaval :**

- Apply Testing process standard for UD composites to woven composite materials, observe the difference
- Develop material model and associated material parameters
- Implement material behavior using user material within ABAQUS
- Validate models results against experimental results using standard specimens (3PB, OCT, SBS, drop tower LVI, HVI, etc.)
- Try to apply inverse identification process for predictive model parameters

Introduction

- **Laboratory M3C Uaval :**
 - Modelling material behavior using **user's material subroutine** with ABAQUS
 - Testing woven composite materials for model parameters
 - Compare model and experimental results
 - **Inverse Modeling:** Try to obtain a model to replicate the same material behavior

Introduction: Timeline for some tests

Tests	A13	W14	S14	A14	W15	S15	A15	W16	S16	A16	W17
Part 1: Characterization tests											
1.1 Quasi-static, low and high strain rate., out-of-plane + in-plane compression	X	X	X	x	x						
1.2 Fracture tests for delamination behaviour	X	X	X	X							
1.3 Cyclic loading for plasticity	X	X	X								
Part 2: Validation tests											
2.1 Low velocity impact on flat panel (hemispherical impactor)											
2.1.1 Postmortem C-scan analysis			X	X	X	X	X	X			
2.2 Three-points bending tests on coupons											
2.1 Short Beam Shear Test			X	X				x	x	x	
2.3 OverHeight Compact Ternsile tests						X	X	x	x	x	x
Part 3: Bird impact, Hail Impact, Crash tests		X	X	X	X				x	x	x

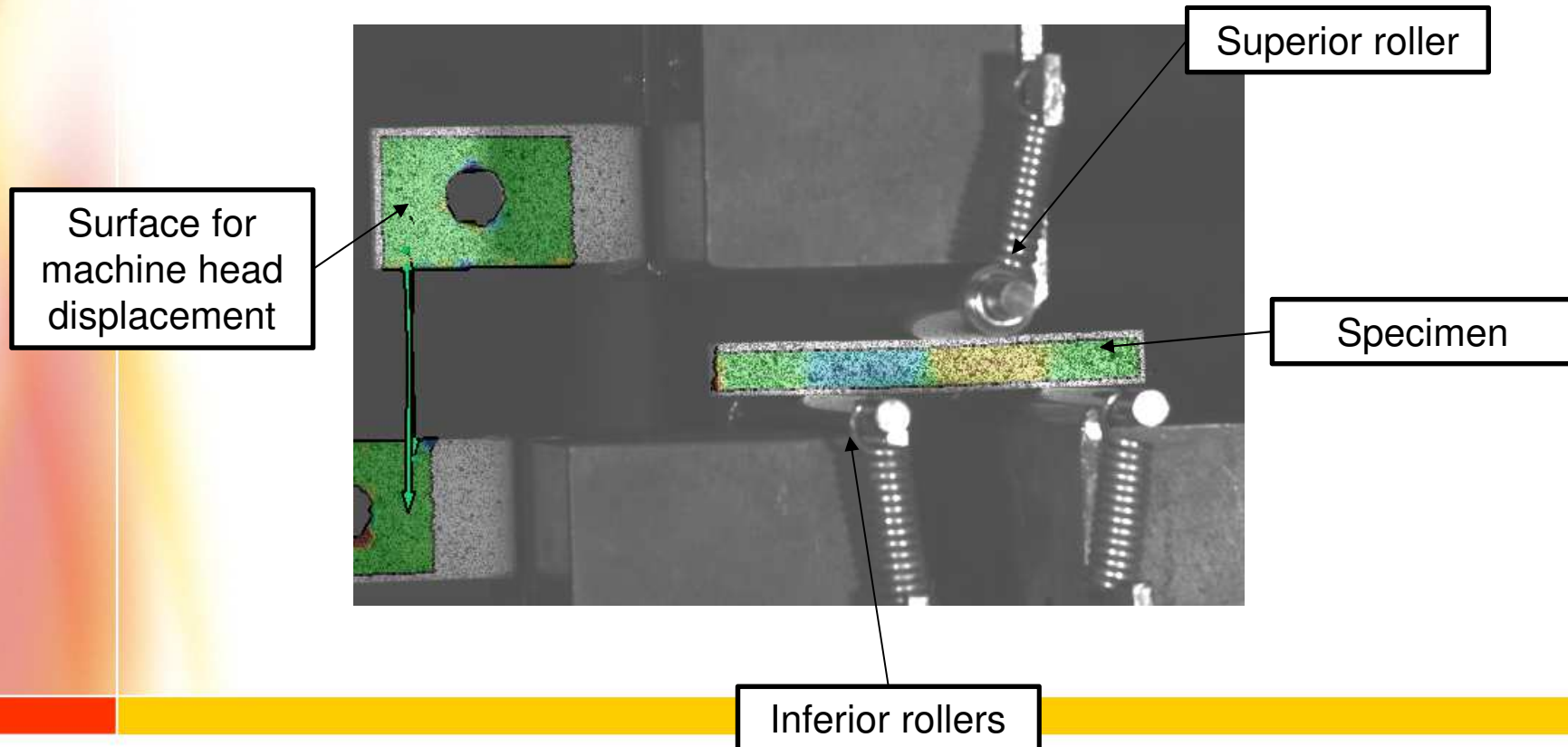
Material tested

- Woven composite material :
 - Carbon fibers (woven pattern)
 - Polymer epoxy matrix
 - Fabrication in autoclave in this case
 - 28 plies material, layup [0,90]14s
 - Material used for aerospace structures

Testing and results: focus SBS

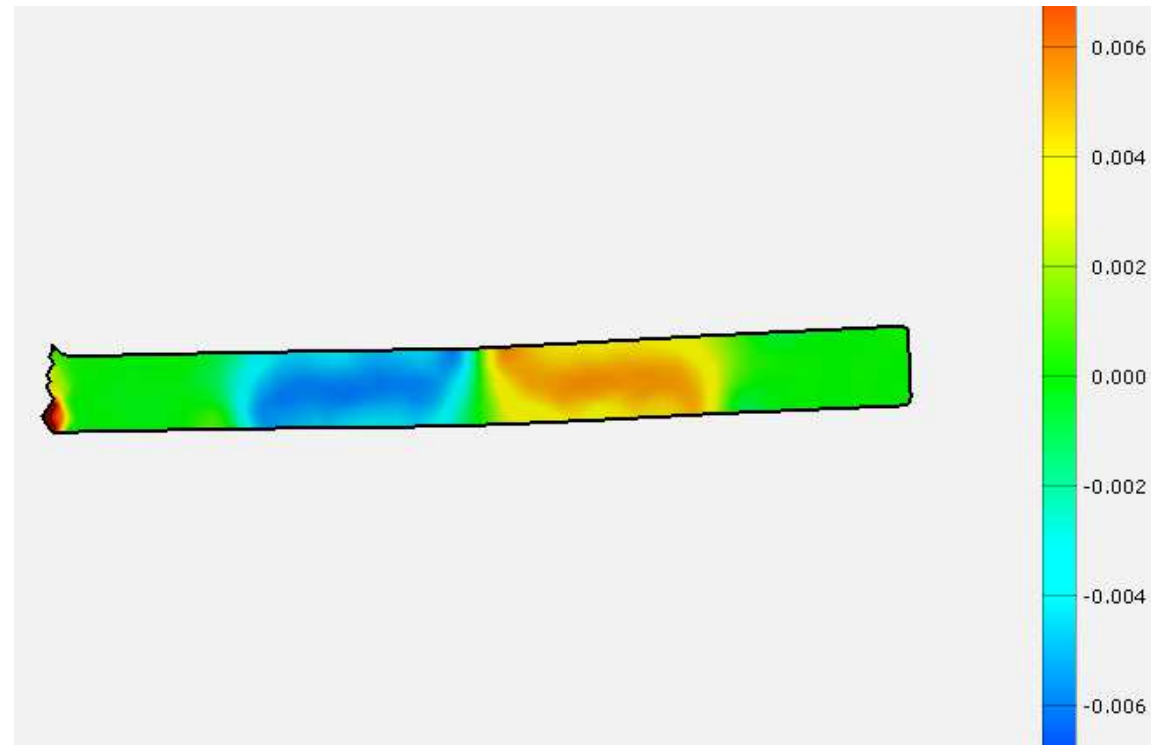
- ASTM D2344 standard used to get shear properties in the out-of-plane direction
- Specimen dimensions slightly modified to get more accurate results (based on experience)
5.7 mm X 5.7 mm X 40 mm
- Superior roller : 6.35 mm
- Inferior roller : 3.175 mm
- Distance between rollers : 22.8 mm (4 x thickness)
- Standard setup from ASTM D2344
- Parameters identified in this test : maximum shear stress and strain and elastic shear modulus:
- Use virtual fields methods

Testing and results : ARAMIS set up



Testing and results: ARAMIS DIC

- Experimental results (epsilon 13)

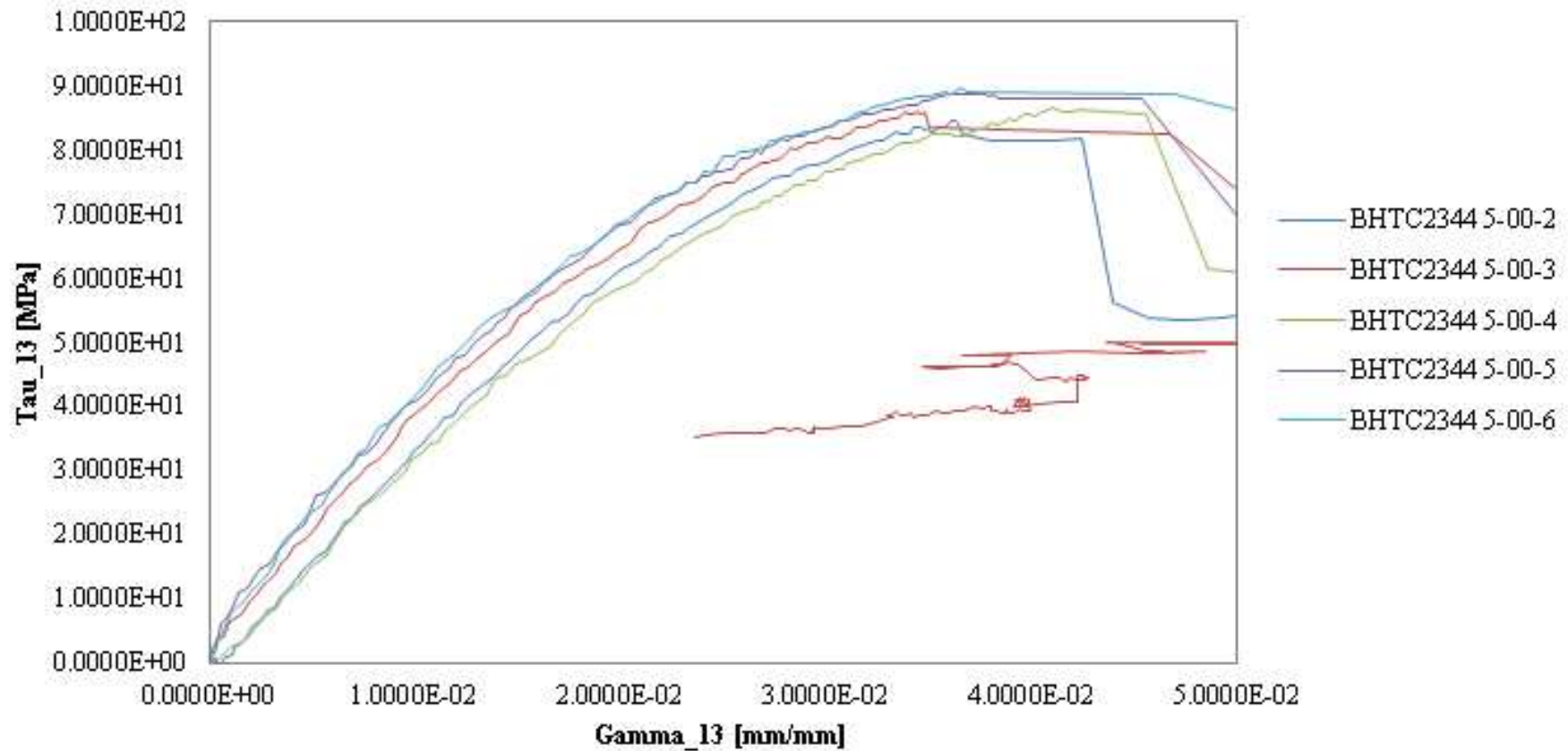


Testing and results

- Experimental results (epsilon 13) on the neutral axis
- Some discontinuities because of the camera noise



Testing and results: (transverse shear stress vs shear strain curves → plasticity or Ramberg-Osgood model can be used)



Testing and results

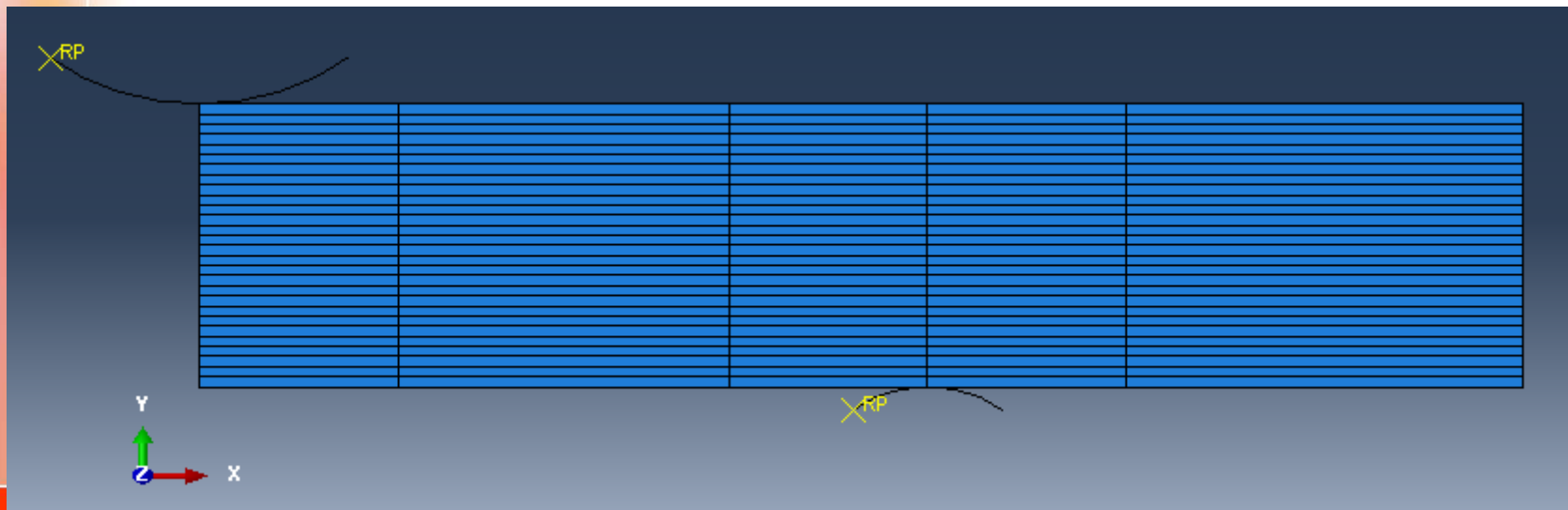
Specimen	Ultimate Shear Strength 13 [MPa]	Ultimate Shear Strain (gamma_13) [%]	Elastic Shear Modulus [GPa]
2	84.47	3.61	3.40
3	85.86	3.45	3.59
4	86.38	4.11	3.27
5	88.73	3.69	3.73
6	89.50	3.67	3.95
Mean Value	87.00	3.70	3.59
Std	2.07	0.244	0.268
CV %	2.39%	6.60%	7.48%

Finite element modelling

- User material **3D-ULavalPLYFabric**-(improved MAT162 from LS-DYNA) implemented in ABAQUS
- 40 material parameter for an explicit analysis
- Parameters from testing and from a mathematical formulation
- Mass scaling used for a faster analysis
- C3D8R solid elements
- Mesh refined near contact surfaces
- Elastic model used for parameter identification, more effective but can also be used with a VUMAT

Finite element modelling

- Geometry : quarter of a specimen with boundary conditions for efficient calculations
- Rigid rollers with reference points for load and displacement measurements



Finite element modelling

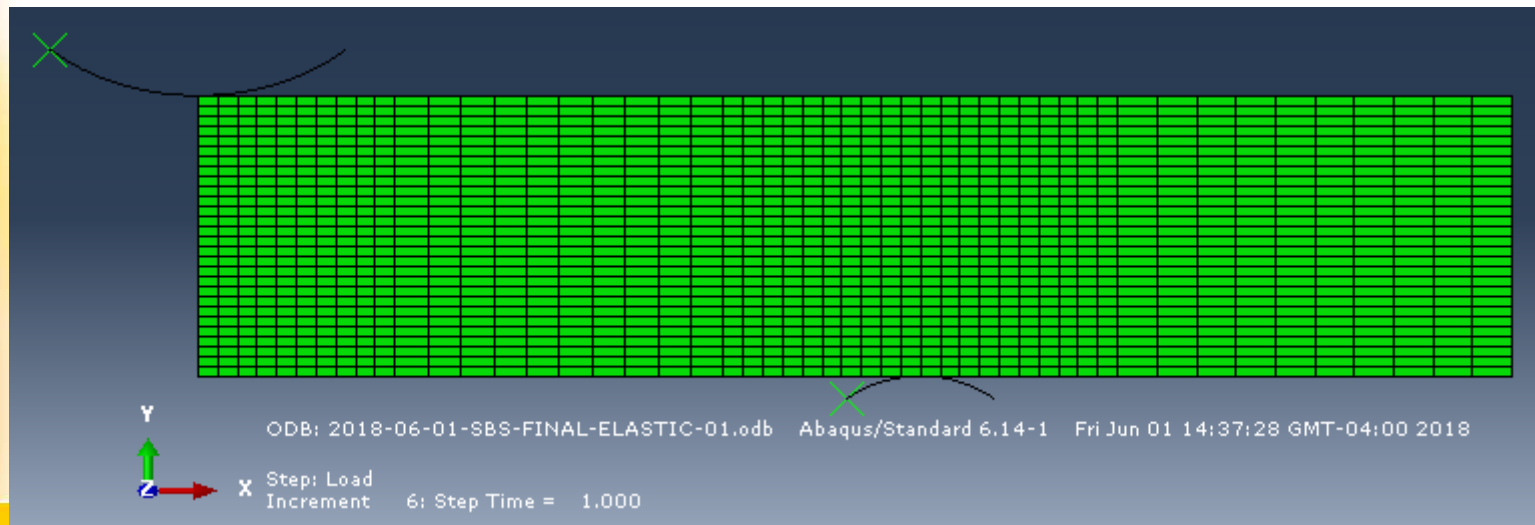
- Boundary conditions and loads :
 - Superior roller : displacement of 1 mm in the y direction
 - Inferior roller : encastré
 - Symmetry in the x and y directions to reduce calculations

Finite element modelling

- Model interactions
 - Slight friction on rollers and hard contact with the specimen
 - Cohesive surfaces between plies
 - Gf Parameters obtained from experimental testing (Beckelynck, 2016)
 - More effective than cohesive elements
 - Can be used to get delamination when the material fails

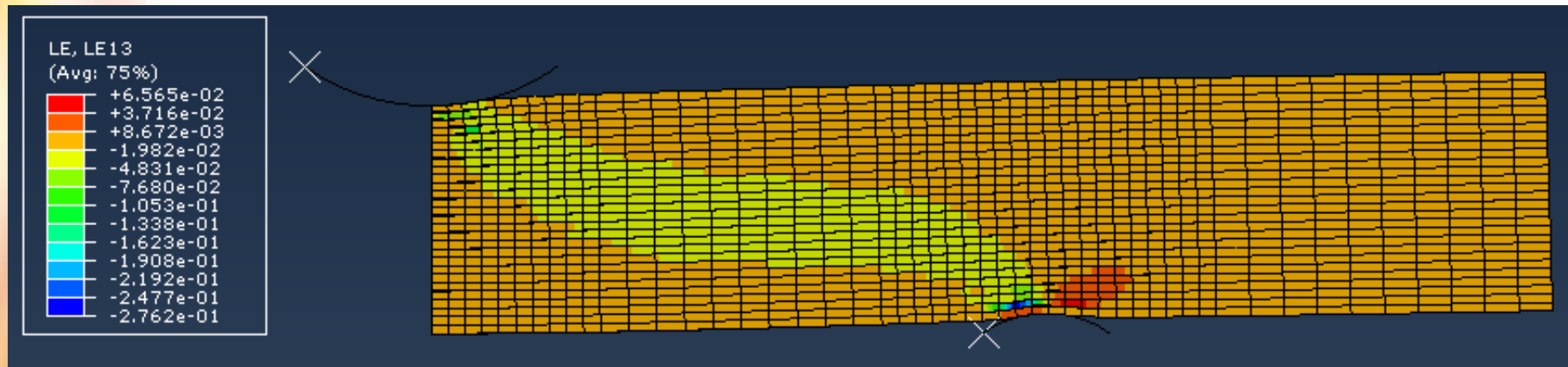
Meshing

- 10 elements per partition
- Finer mesh near rollers
- Elements seem homogeneous, reduce stress concentration



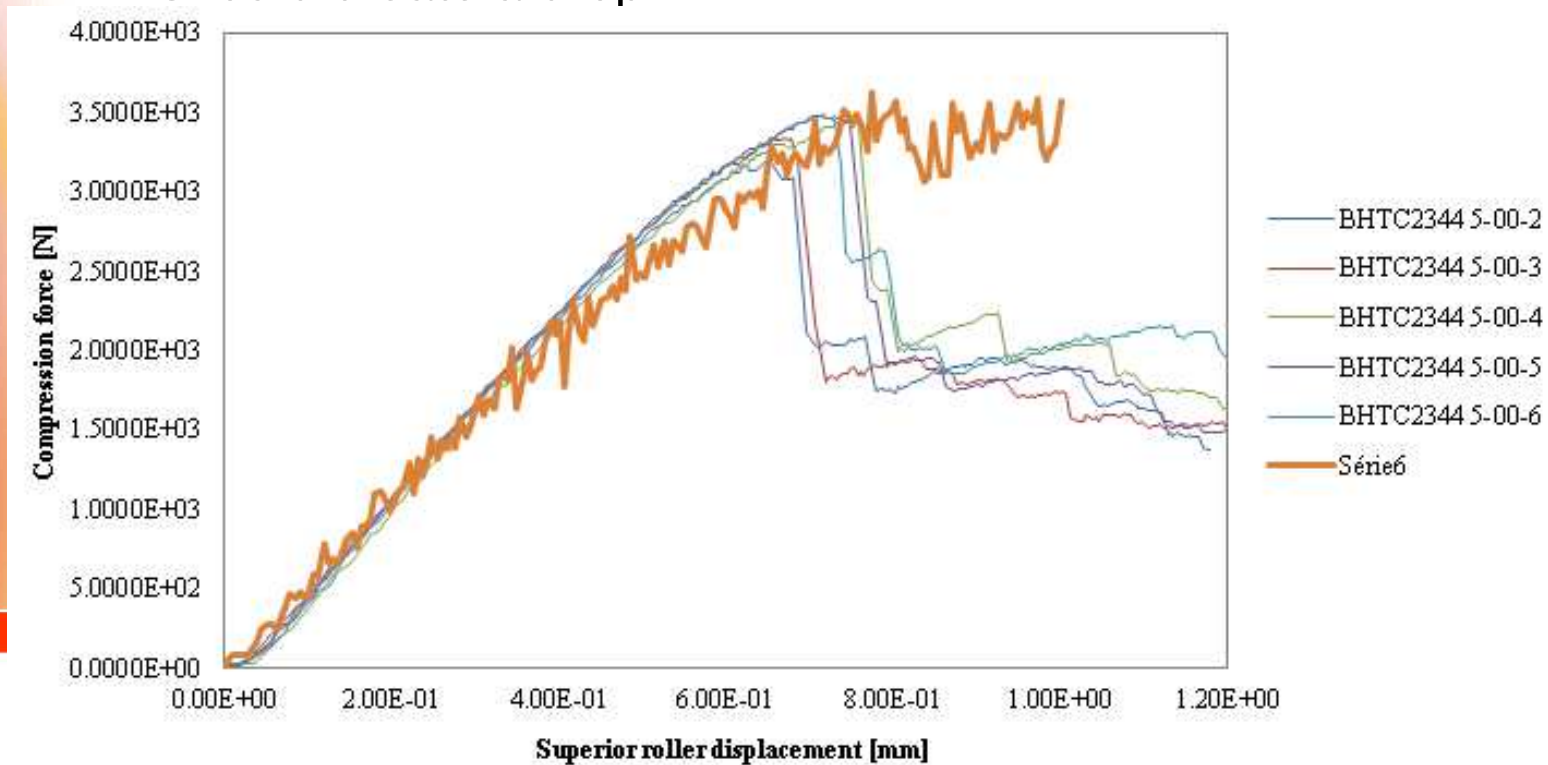
FEA results

- With a user material 3D-ULAVAL-PLYFABRIC model162
- Shear strain distribution (gamma 13)



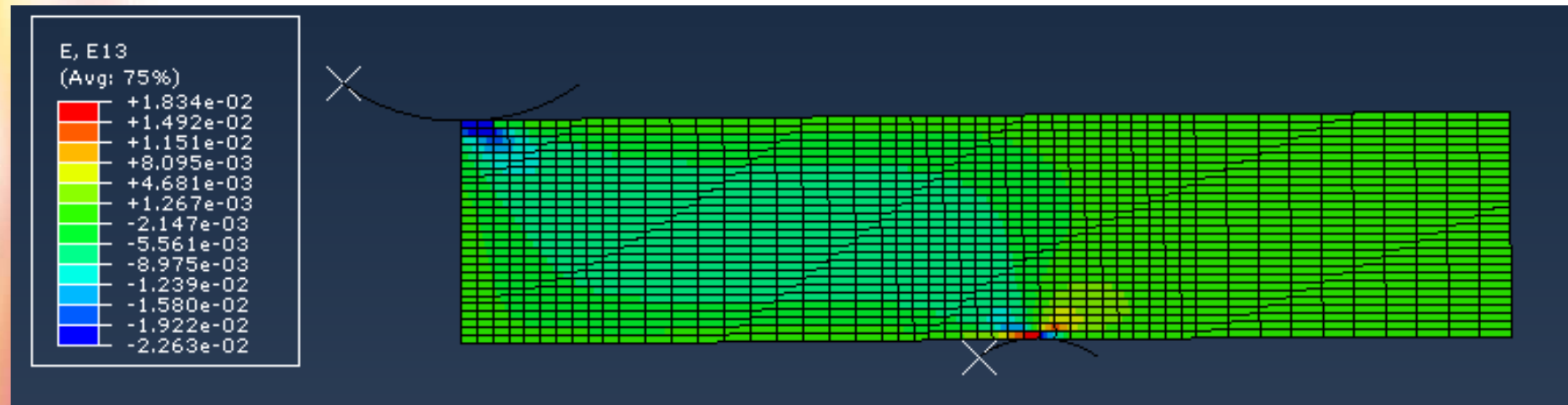
FEA results

- With a user material 3D-ULAVAL-PLY-FABRIC model162 (force-displacement)
- Slope and damage seem good, but delamination value should create a drop



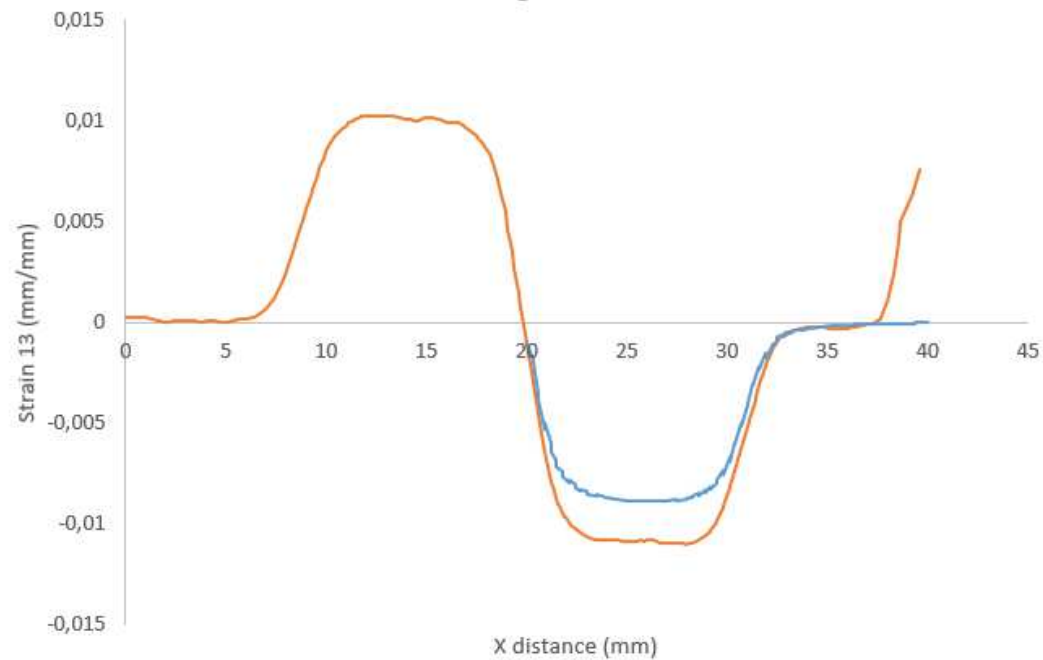
FEA results

- Assuming an elastic material behaviour



FEA results

- With an elastic material, results in blue color compared with experimental data
- Some differences between the standard and the model



Inverse problem

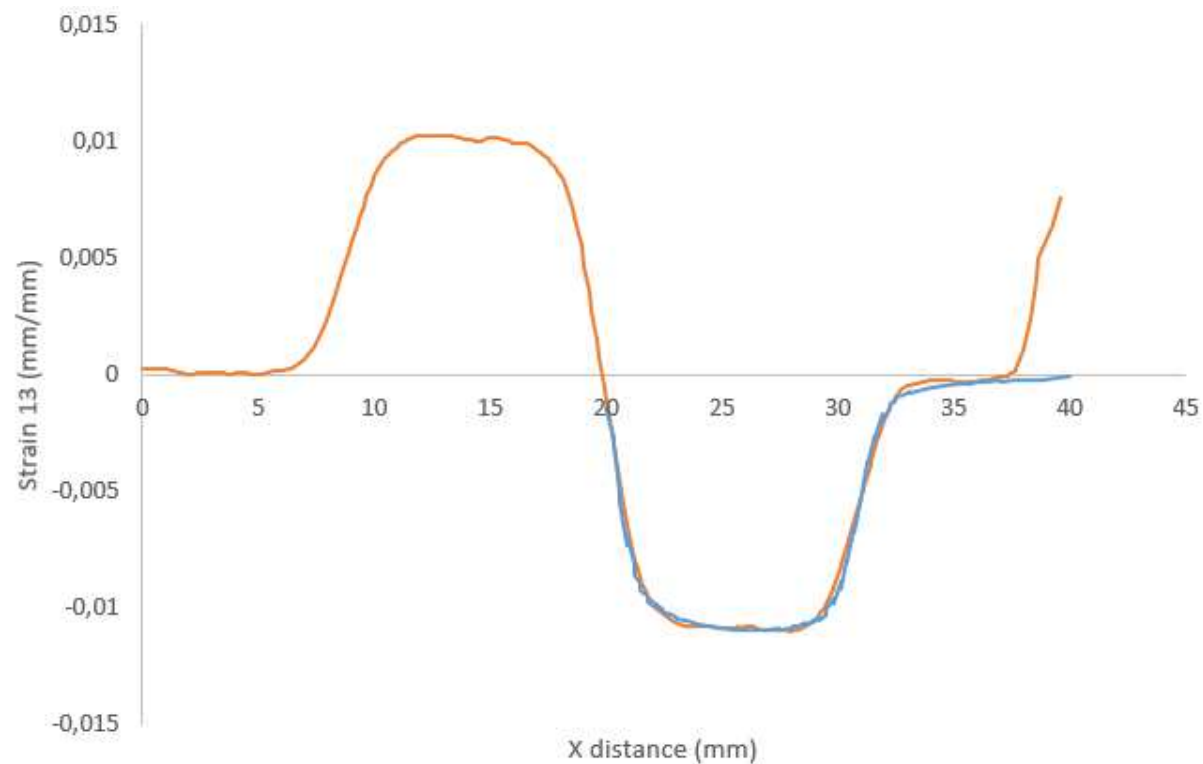
- ASTM standard uses beam theory for the stress values
- A woven composite can differ from unidirectional material
- Using the digital image correlation system → Inverse problem
- Goal : Is it possible to Get the same results as the experimental results
- In our case, strain is used for the identification, other variables can be used as well

Parameter identification algorithm

1. Use a first approximation for properties (ASTM D2344)
2. Run FEA from the given properties
3. Compare experimental results and FEA results
4. Perform a **nonlinear optimisation technique** to define a parameter variation
5. Add the variation to the properties
6. Loop the steps 2 to 5 as long as the convergence parameter is not satisfied
7. Get the identified properties

Results from identification

- Elastic modulus : 2.5 Gpa compared to 3.5 Gpa previously **after using 3D-ULAVAL-PLY-FABRIC**
- Strain distribution :



Conclusion

- Model developed to get the same material behavior with a finite element analysis
- Short beam strength test for shear parameters in the out-of-plane direction
- Difference between theory and experimental properties values
- Inverse identification to get the real values from the strain field
- FEA can estimate more accurately the experimental results
- Further work to improve modeling process

Thank you for your attention

Questions or comments?

References

ASTM International (2007). D2344 : Standard test method for short-beam strength of polymer matrix composite materials and their laminates.

Forestier, R. (2004). Development of a parameter identification method by inverse analysis coupled with a 3D finite element model.

Gauthier, L. (2010). Modelling of High Velocity Impact in Composite Materials for Airframe Structures Application. PhD thesis, Laval University.

Hrairi et al. (2011). Modeling the powder compaction process using the finite element method and inverse optimization.

Van der Vossen, B. (2014). Spatial variability of stiffness fiber reinforced composites in short beam shear test specimens.

Yihong, H. et al. (2012). Characterization of nonlinear shear properties for composite materials using image correlation and finite element analysis.

Zobeiry, N. (2010). Extracting the Strain-Softening Response of Composites Using Full-Field Displacement Measurement. PhD thesis, University of British Columbia